## Stayton Veterinary Hospital

## PRELIMINARY STORMWATER REPORT

April 2<sup>nd</sup>, 2024 1308 N 1<sup>st</sup> Ave Stayton, Oregon 97383



RENEWAL DEC. 31, 2024

## PREPARED BY:



Site Name:	Stayton Veterinary Hospital
Property Location:	1308 N First Ave 9S-01W-10AC Lots 2400, 2500, 2600, 2700, and 2800.
Site Property Owner/Applicant:	Dark Horse Enterprise LLC C/O Dr. Michael Reynolds 1308 N 1 <sup>st</sup> Ave Stayton, OR 97383
Engineer:	Udell Engineering & Land Surveying, LLC 63 East Ash St. Lebanon, Oregon 97355 Andrew Rappé, PE (541) 451-5125 andrew@udelleng.com

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## 1.0 Purpose of Report

Udell Engineering and Land Surveying, LLC, abbreviated UELS, was consulted by the applicant, Dr. Michael Reynolds, to develop a preliminary Stormwater Report for the proposed development located at 1308 N 1<sup>st</sup> Avenue in Stayton, Oregon. The proposed development includes the expansion of the existing hospital building and parking lot across the full city lot. The applicant currently owns all 5 lots on the block and is in the process of consolidating the lots into one.

The purpose of this report is to demonstrate that the tentative improvements are capable of conforming with the City of Stayton post-construction stormwater management standards. UELS followed Division 6 of the City of Stayton Public Works Design Standards (Division 6) to provide water quality and water quantity for the proposed development.

## 2.0 Site Description

The project is currently located across 5 parcels on a 0.96 acre block between 1<sup>st</sup> Ave and 2<sup>nd</sup> Ave to the west and east, and E Pine St and E Hollister St to the north and south. The southern two lots consist of the existing veterinary hospital building and parking lot. The lots to the northwest consist of single family residences. The lot to the northeast is vacant, but was formerly a residence. A public alley running north and south through the block was vacated in 2023. The 5 parcels are proposed to be consolidated into one through a separate land use application.

Stormwater runoff from the site is shed to the surrounding right-of-way, with public stormdrain mains located in Pine, Hollister, and 1<sup>st</sup> Ave. The property is currently served by power, gas, sewer, and water. Service lines to the former residences will be removed and/or abandoned.

## 3.0 Proposed Stormwater Facility Improvements

Water quality treatment will be provided by an onsite water quality basin. The basin will infiltrate most of the incoming water underground. During extreme rain events, the basin will top an overflow inlet and discharge to the public storm drain system at the NE corner of N First and E Hollister. The system is designed to limit post-developed to pre-developed peak runoff rates for the 2, 5, 10, 50, and 100-year 24-hour storm events. Additionally, the post-developed 25-year storm event is limited to well below the 10-year pre-developed peak runoff rate.

## 4.0 Design Methodology and Calculations

#### 4.1 Water Quality

For Water Quality sizing, UELS followed the City of Portland 2020 Stormwater Management Manual (PSWMM) as referenced by Division 6. The Water Quality basin is designed using the Performance Approach by incorporating the water quality storm event into the overall hydrology model as described in section 4.2.

#### 4.2 Water Quantity

For water quantity (flow control) calculations, UELS used the Santa Barbara Urban Hydrograph method to build a hydrologic model using Hydrocad software Version 10.00-24: The software model for this project is comprised of 2 types of nodes: sub-catchments and ponds.

Sub-catchment nodes model the basin areas of land that receive rainfall during a storm. They generate runoff hydrographs based on several factors, including the runoff curve numbers, time of concentration, and design storms. For this model, UELS used curve numbers from the PSWMM into the software for the varying types of area with the contributing basin, pre-developed and post-

developed. For the post-construction basin, UELS used the software to calculate the time of concentration for the drainage basin. The 24hr design storm values used in the model were taken from Division 6 and are shown in Table 1 below.

In this hydrologic model, UELS used a pond node to model the stormwater management. The pond volume includes the above-ground basin area as well as the below-ground void spaces in the soil media filtration layer. Runoff that is not infiltrated into the groundwater table overflows into an overflow inlet. The inlet acts as a weir during large storm events and helps to limit the peak runoff flows.

The following table displays the input parameters that UELS used in the Hydrocad model. See the proposed Preliminary Development plans in Appendix A for details of the post-construction site.

Table 1, Input Parameters used for Hydrologic Analysis

Table 1, input 1 arameters used for frydrologic Amarysis									
Parameter	Value	Source							
Curve Numbers	Varies	PSWMM							
Rainfall Distribution	Type 1A	SCS/NRCS							
Hydrologic Soil Group	В	NRCS Web-Soil Survey							
Design Infiltration Rate*	3.7 in/hr	NRCS Web-Soil Survey							
Water Quality, 24 hr Design Storm	1.61 in	Div. 6 Table 603.02.C.3							
2yr., 24 hr Design Storm	2.50 in	Div. 6 Table 603.02.C.3							
5yr., 24 hr Design Storm	3.00 in	Div. 6 Table 603.02.C.3							
10yr., 24 hr Design Storm	3.50 in	Div. 6 Table 603.02.C.3							
25yr., 24 hr Design Storm	4.00 in	Div. 6 Table 603.02.C.3							
50yr., 24 hr Design Storm	4.50 in	Div. 6 Table 603.02.C.3							
100yr., 24 hr Design Storm	4.60 in	Div. 6 Table 603.02.C.3							

<sup>\*</sup>The design infiltration rate is based on the saturated hydraulic conductivity as identified by NRCS and includes a factor of safety of 4.0. Prior to final engineering, in-situ infiltration tests will be performed on site.

The following table displays the results of the hydrologic calculations. See Appendices D & E for all input and output data from the Hydrocad model.

Table 3, Comparison Table of Pre-Development to Post Development Release Rates

Storm Event	Pre-	Post-Developed,	Post-Developed,	Peak	Storage	
	Developed	w/o Flow Control	w/ Flow Control (cfs)	Elevation (ft)	Volume* (cf)	
	(cfs)	(cfs)				
WQ Storm	0.009	0.267	0.000	456.03	188	
2yr24hr	0.041	0.431	0.000	456.75	593	
5yr24hr	0.089	0.522	0.000	457.04	912	
10yr24hr	0.146	0.613	0.000	457.34	1,291	
25yr24hr	0.208	0.704	0.095	457.53	1,568	
50yr24hr	0.276	0.794	0.283	457.57	1,623	
100yr24hr	0.290	0.812	0.335	457.58	1,635	

<sup>\*1,1776</sup> cf provided

## 5.0 Conveyance System

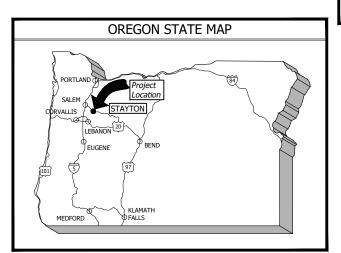
Storm pipe sizing will be evaluated fully during final engineering using the Rational Method per City of Stayton Public Works standards.

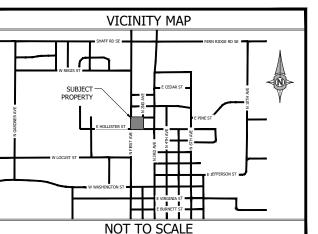
## 6.0 Conclusion

UELS prepared this preliminary stormwater report for the proposed development to generally conform with the City of Stayton, Division 6 Stormwater Management design standards. The body of this report provides detailed parameters and design criteria that demonstrate conformance with the design standards. Based on the information within this report and the analysis provided, UELS believes that the stormwater management plan for the proposed development meets or exceeds City of Stayton Stormwater Management Public Works Design Standards.

## APPENDIX A PRELIMINARY SITE DEVELOPMENT PLANS

## PRELIMINARY SITE IMPROVEMENTS STAYTON VETERINARY HOSPITAL 1308 NORTH 1ST STREET AVE STAYTON, OREGON





#### SHEET INDEX

C102 - SITE PLAN

C200 - GRADING AND DRAINAGE PLAN

C100 - COVER SHEET

C101 - EXISTING CONDITIONS/DEMO PLAN

C300 - UTILITY PLAN

#### SHEET REVISIONS

#### **PROPERTY**

TAX MAP: 9S-01W-10AC TAX LOTS: 2400, 2500, 2600, 2700, & 2800 TOTAL NET AREA: 0.96 ACRES

SITE ADDRESS:

1308, 1328, & 1336 N FIRST AVE 181 & 190 E HOLLISTER ST STAYTON, OR 97383

#### APPLICANT/OWNER

DARK HORSE ENTERPRISE LLC C/O MICHAEL REYNOLDS 1308 N 1ST AVENUE STAYTON, OR 97383 (503) 769-7387

#### **DESIGN TEAM**

#### CIVIL ENGINEER

UDELL ENGINEERING AND LAND SURVEYING, LLC 63 E. ASH STREET LEBANON, OREGON 97355 (541) 451-5125 CONTACT: ANDREW RAPPÉ, PE

#### **SURVEYOR**

UDELL ENGINEERING AND LAND SURVEYING, LLC 63 E. ASH STREET LEBANON, OREGON 97355 (541) 451-5125 CONTACT: KYLE LATIMER, PLS

#### **ARCHITECT**

MD ARCHITECTS
11416 98TH AVE NE, SUITE 200
KIRKLAND, WA 98034
(425) 823-2244
CONTACT: NICHOLAS RENO
NICHOLASR@MDARCHITECTS.COM

#### LANDSCAPE ARCHITECT

LAURUS DESIGNS 1012 PINE STREET SILVERTON, OREGON (503) 784-6494 CONTACT: LAURA ANTONSON, RLA, ASLA

#### LIGHTING DESIGNER

PURE ENERGY GROUP 139 ANKENY HILL RD SE JEFFERSON, OR 97352 (541) 936-0980 CONTACT: TRAVIS SHEFFIELD TRAVIS@PUREENERGY.GROUP

# SHEET COVER 3

STAYTON VETERINARY HOSPITAL 1308 N. FIRST AVE STAYTON OR 97383

STAYTON VETERINARY HOSPIT C/O MICHAEL REYNOLDS 1308 NORTH FIRST AVENUE STAYTON, OR 97383 (503) 769-7387

UDELL ENGINEERING

AND

LAND SURVEYING, LLC

63 EAST ASH ST.

LEBANON, OREGON 97355

(541) 451-3125 PH.

(541) 451-3166 FAX

CLIENT:

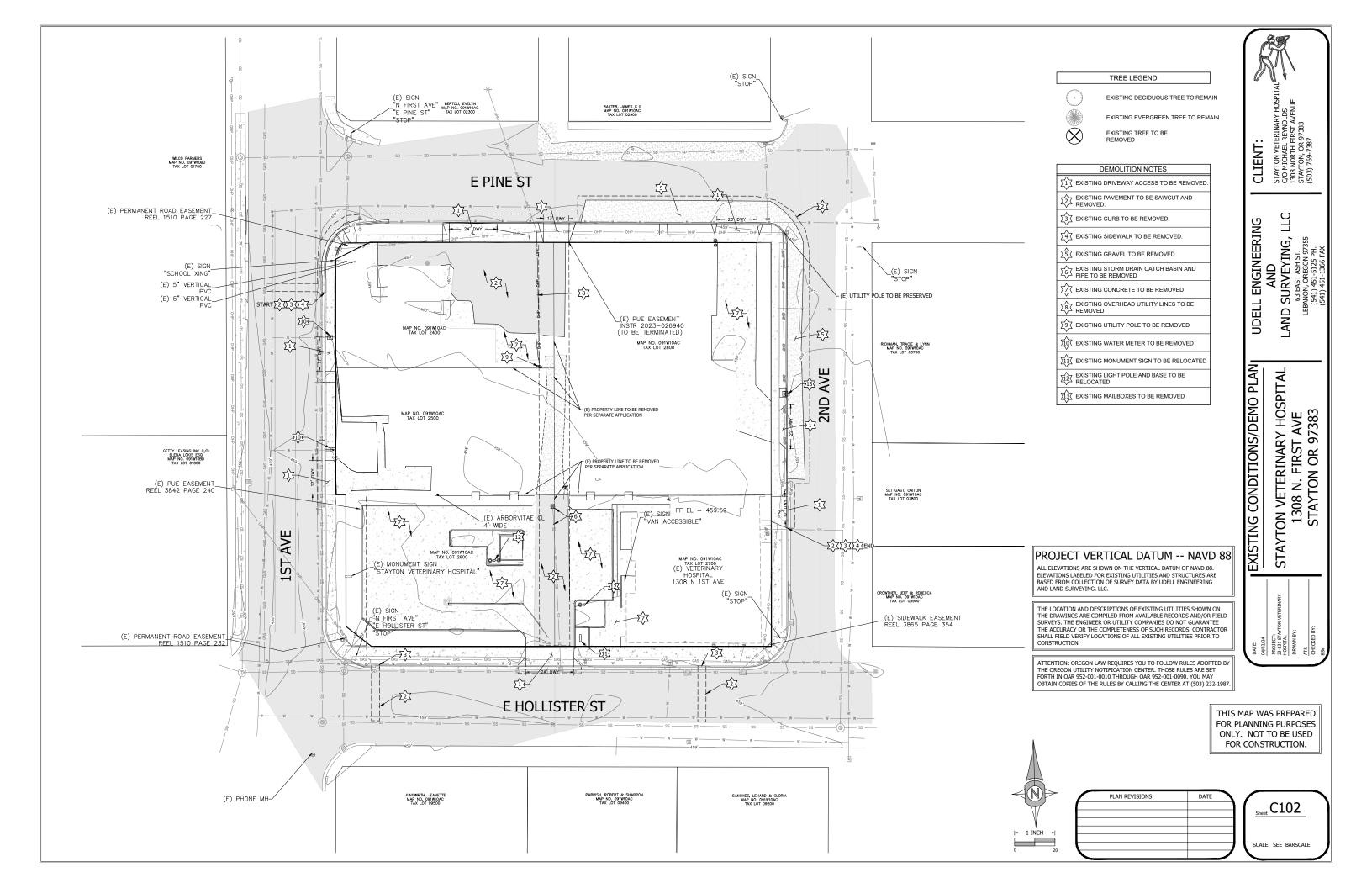
THIS MAP WAS PREPARED FOR PLANNING PURPOSES ONLY. NOT TO BE USED FOR CONSTRUCTION.

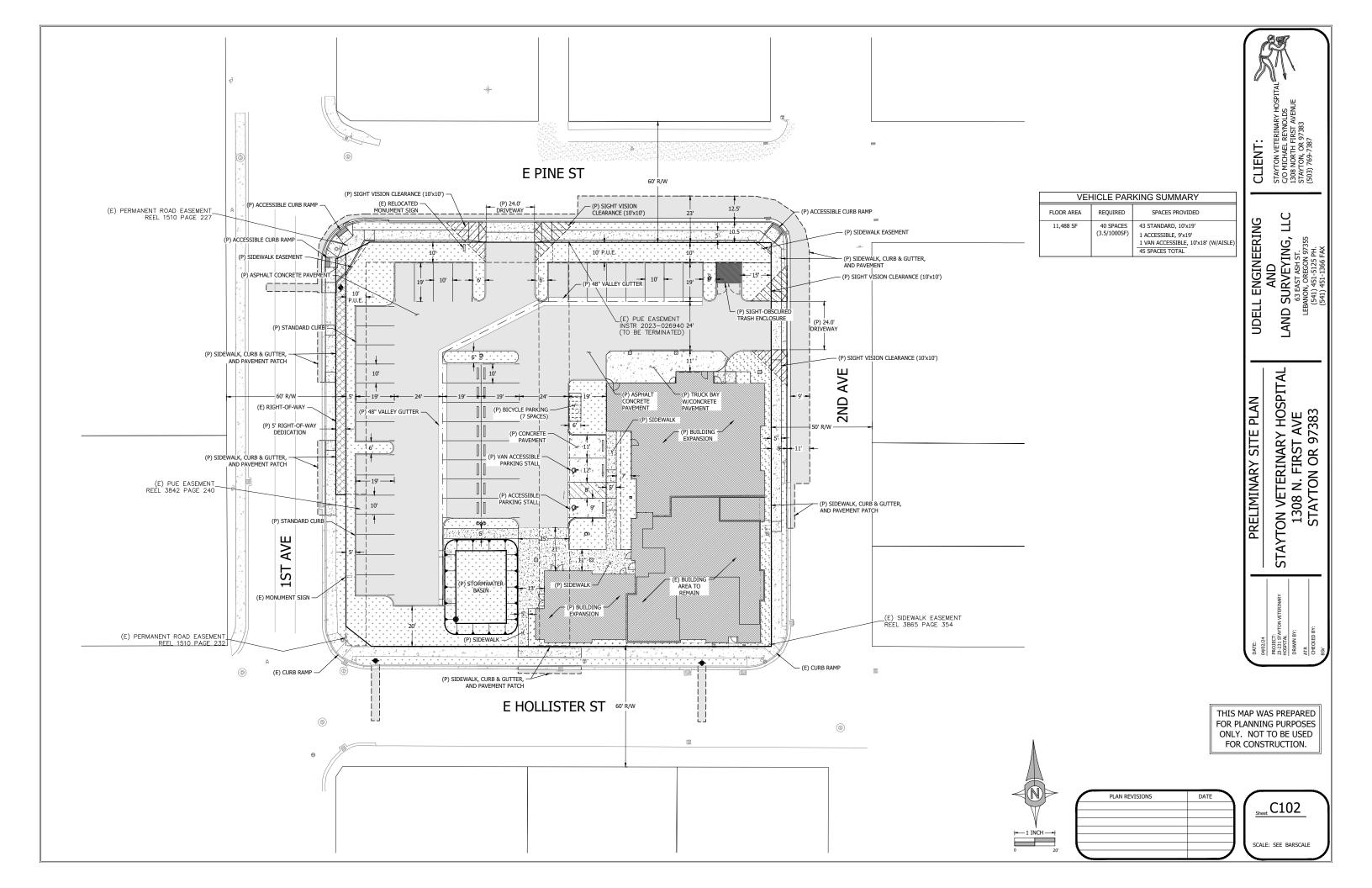
PLAN REVISIONS

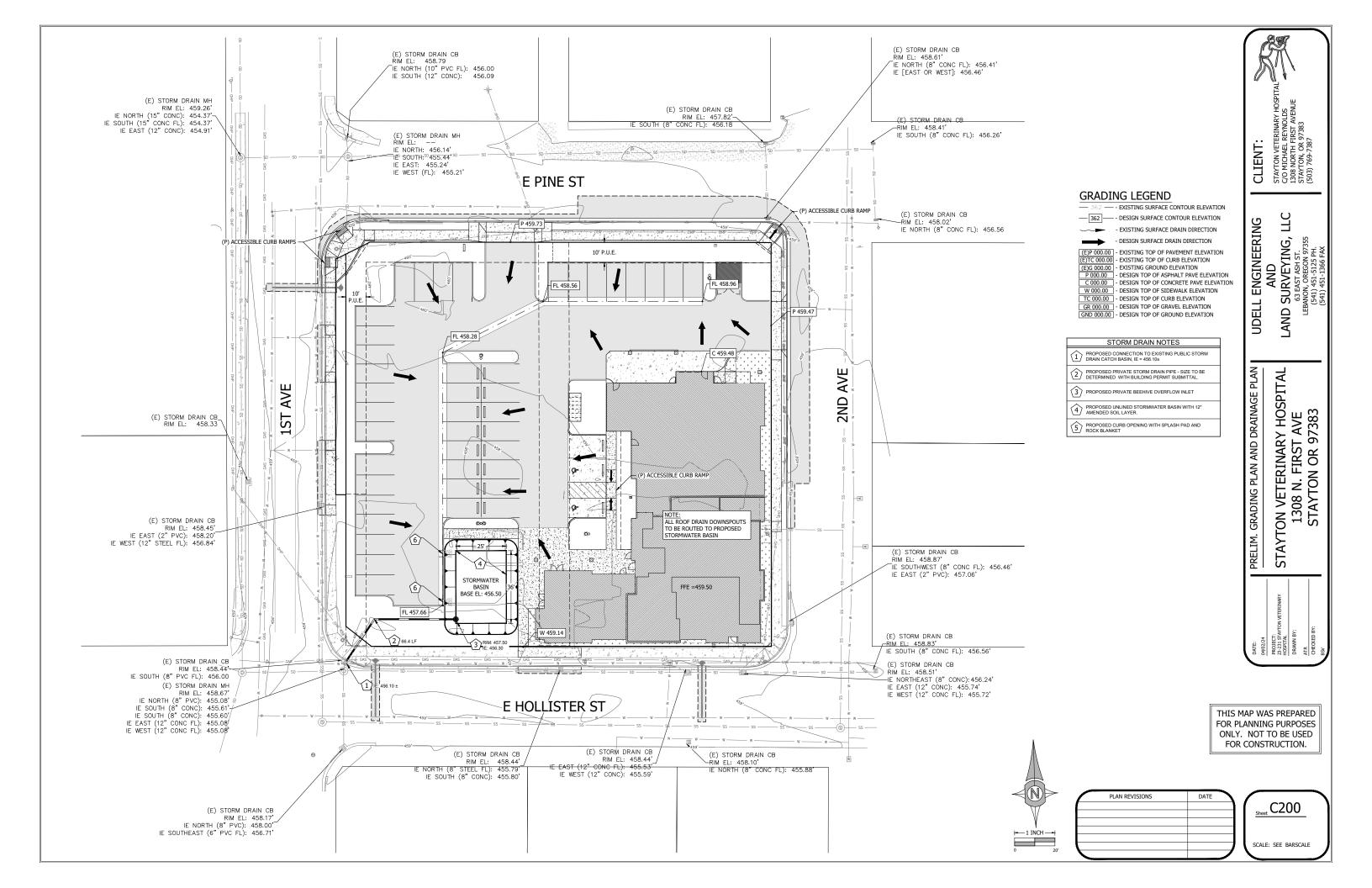
 $\underline{_{\text{Sheet}}\,C}100$ SCALE: SEE BARSCALE

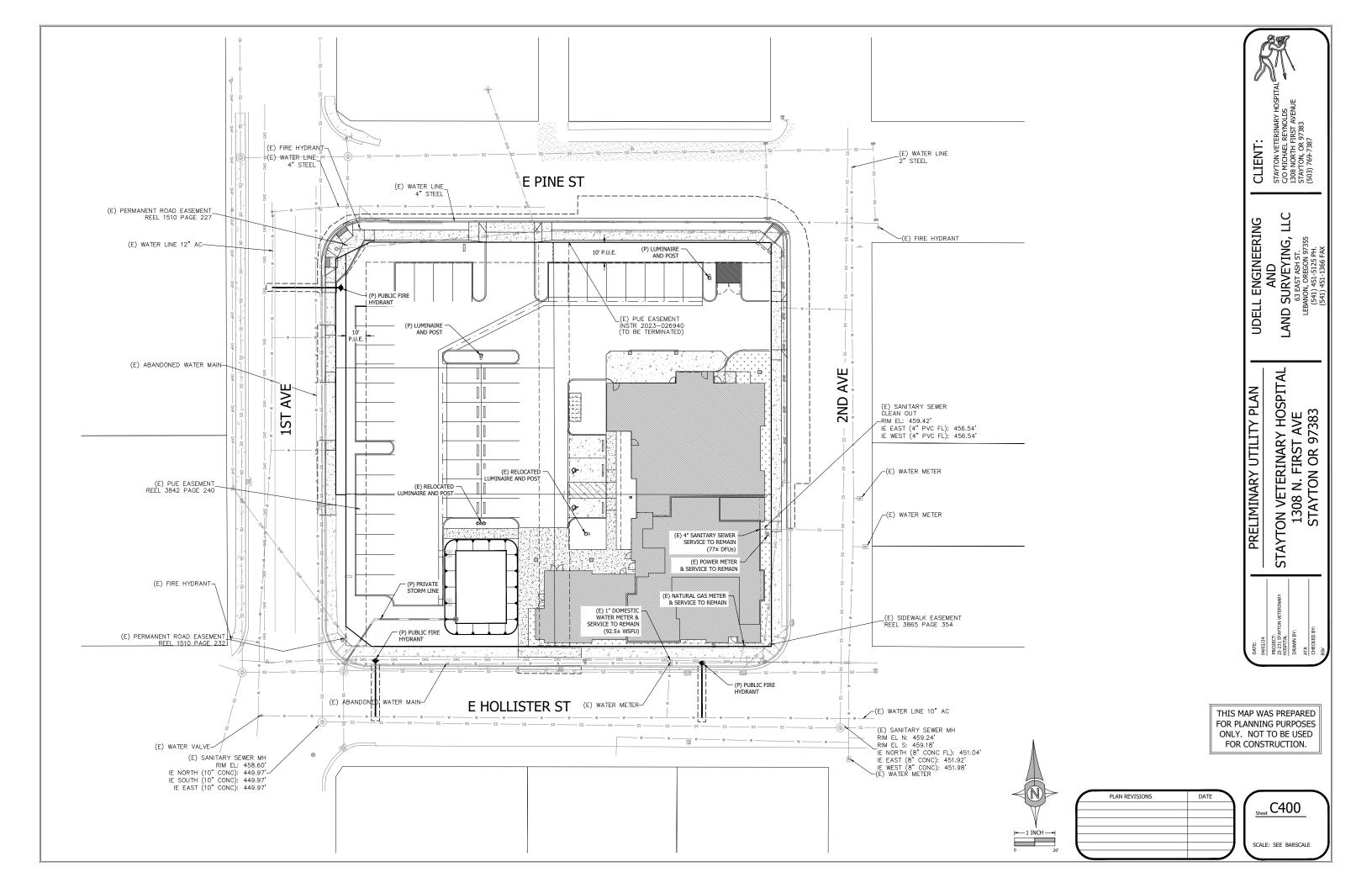
EVICTING	SYMBOL LEGEND	\ DDF	REVIATIONS LEGEND	CD^	GRADING LEGEND		
EVIOLING	1 3 I MIDUL LEGEND	ADDR	ENTATIONS FEGEIND	GRA	DING FEGEIND		
<u>A</u> ⊠	- EXISTING CONTROL POINT - EXISTING GAS VALVE	SS SD MH	- SANITARY SEWER - STORM DRAIN - MANHOLE	-	.00% - SURFACE DRAIN DIRECTION		
			· · · · · · · · · · · · · · · · · · ·	(E)P 00			
-	- EXISTING WATER VALVE	CB CO	- CATCH BASIN	(E)TC 0			
М	- EXISTING WATER METER		- CLEAN OUT	(E)G 00			
Δ.		PP	- UTILITY POLE	P 000	.00 - DESIGN TOP OF ASPHALT PAVEMENT ELEVATION		
(0)	- EXISTING FIRE HYDRANT	IE	- INVERT ELEVATION (FLOW LINE)	C 000	.00 - DESIGN TOP OF CONCRETE PAVEMENT ELEVATION		
6	- EXISTING POWER POLE	FF	- FINISH FLOOR	W 000	0.00 - DESIGN TOP OF SIDEWALK ELEVATION		
_	ENGRETING OF GIVEN ONE SERVICE	R.O.W.	- RIGHT-OF-WAY	TC 000	0.00 - DESIGN TOP OF CURB ELEVATION		
-000	- EXISTING 6' CYCLONE FENCE	FD	- FOUND	GR 000			
	EXISTING 6' WOOD FENCE	CS	- COUNTY SURVEY	GND 00			
x x	EXISTING 6 WOOD PENCE	IR	- IRON ROD				
SD EXISTING SD LINE LOCATE		R	- RADIUS	TW 00	0.00 - DESIGN TOP OF WALL ELEVATION		
	- EXISTING 3D LINE LOCATE	BO	- BLOWOFF				
SS	EXISTING SS LINE LOCATE	S.L.	- STREET LIGHT	DEC	IGN SYMBOL LEGEND		
	ENDING OF LINE LOGINE	TC	- TOP FACE OF CURB	DLS	IGN STRIDGE LEGEND		
w	EXISTING WATER LINE LOCATE	BW	- BACK OF WALK				
	ENDING WITER EINE EOGNE	CL	- CENTERLINE	M	- DESIGN WATER METER		
PH	EXISTING PHONE LINE LOCATE	FH	- FIRE HYDRANT	_			
		CI	- CURB INLET		- DESIGN CURB INLET		
—— UGP ——	- EXISTING UNDERGROUND POWER LOCATE	T.O.P.	- TOP OF PIPE				
		FL	- FLOW LINE		- DESIGN CATCH BASIN		
OHP	- EXISTING OVERHEAD POWER	PUE	- PUBLIC UTILITY EASEMENT				
		EX OR (E)	- EXISTING		- DESIGN DITCH INLET		
GAS	- EXISTING GAS LINE LOCATE	(P)	- PROPOSED		DESIGN DITON INCE!		
сом	EXISTING COMMUNICATION LINE LOCATE	ΡΈ	- PLAIN END		DECICAL CC MANUOLE		
- COM	- EXISTING COMMUNICATION LINE LOCATE	FLGD OR FLG	G - FLANGED	(3)	- DESIGN SS MANHOLE		
356'	EXISTING CONTOUR ELEVATION	MJ	- MECHANICAL JOINT				
		D.I.	- DUCTILE IRON	<b>(</b>	- DESIGN SD MANHOLE		
		W/L	- WATERLINE	Ø	DECICAL MATER VALVE		
		TW	- TOP OF WALL	8	- DESIGN WATER VALVE		
		SDAD	- STORM DRAIN AREA DRAIN		- DESIGN FIRE HYDRANT		

PROJECT LEGENDS









**BEEHIVE INLET - SECTION** 

## **NOTES:**

- 1. SET BEEHIVE RIM ELEVATION AT: CURB AND GUTTER FLOW LINE (FL) ELEVATION, 2" BELOW LOWEST SIDEWALK ELEVATION, OR 2" BELOW LOWEST TOP OF CURB ELEVATION. USE WHICHEVER IS LOWEST.
- CONSTRUCT CONCRETE BASE SLOPED TO DRAIN. CONCRETE BASE SHOULD HAVE A MINIMUM THICKNESS OF 6" AT DRAIN PIPE INVERT.
- 3. IF CONNECTING TO A COMBINATION SEWER MAINTENANCE HOLE INSTALLATION OF A SWING-CHECK TYPE BACKWATER VALVE OR APPROVED EQUAL IS REQUIRED TO PREVENT ODOR EMISSIONS. INSTALL PER MANUFACTURER'S RECOMMENDATION.
- IF BEEHIVE INLET IS LOCATED IN A LINED FACILITY, THEN ATTACH LINER TO STRUCTURE USING STAINLESS STEEL SHEAR BANDS.
- INSTALL OLYMPIC FOUNDRY INC. MH25 BEEHIVE GRATE WITH MH30 24x4 REVERSIBLE RING, OR APPROVED EQUAL.
- CAST IRON ASTM A48 CL30 5.1.
- 5.2. 276 OPEN SQUARE INCHES
- 5.3. BOLT GRATE TO FRAME IN 2 PLACES WITH \( \frac{3}{8} \)" SS HEX BOLT. COUNTER SINK NOT REQUIRED.
- BOLTS TO HAVE ANTI-SEIZE THREAD LUBRICANT APPLIED AT INSTALLATION.

The selection and use of this Standard Drawing, while designed in accordance with generally accepted engineering principles and practices, is the sole responsibility of the user.



**Bureau of Environmental Services** CITY OF PORTLAND, OREGON

Chief Engineer

STANDARD DRAWING Title

**BEEHIVE INLET** 

All material and workmanship shall be in accordance with the City of Portland Standard Construction Specifications.

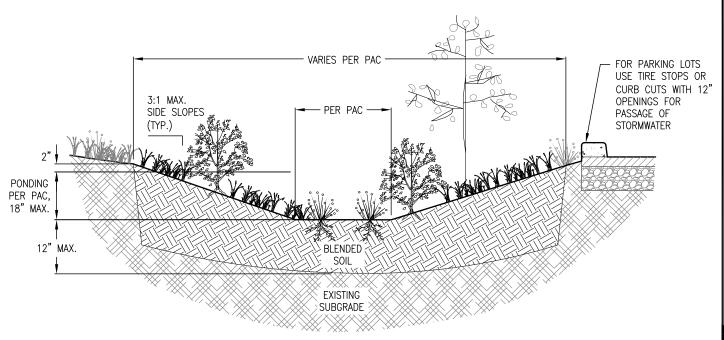
Effective Date: 07-31-20

Calc. Book No.: N/A

Standard Drawing No.

Baseline Report Date: N/A

P-309



- Detail intended as an example. Detail must match PAC assumptions and/or design report.
- Setbacks: 5' from property lines except next to right-of-way; 10' from building foundations.
- Rock Gallery/Storage Layer, as required: Size per the PAC. Construct rock galleries of  $\frac{3}{4}$ " washed drain rock overlain by a 3-4" filter layer of  $\frac{1}{4}$ " No.10 washed angular aggregate. Alternative configurations and materials such as cellular storage systems, drainage mats, and non-standard aggregates may be used under the Performance Approach, with BES approval.
- Overflow: Overflow elevation must allow for 2" of freeboard, minimum. Protect from debris and sediment with strainer or grate.
- 5. Blended Soil: Use BES standard soil blend for stormwater facilities (SWMM Section 6.3) unless otherwise approved. Install minimum of 12" on native soil. Install minimum of 24" if there's a drainage layer or storage layer below the imported soil.

- Vegetation: Refer to plant list in SWMM Section 3.5. Minimum container size is 1 gal. Number of plantings per 100sf of facility
  - Zone A (wet): 80 herbaceous plants OR 72 herbaceous plants and 4 small shrubs.
  - Zone B (moderate to dry): 7 large or small shrubs AND 70 groundcover plants.

The delineation between Zone A and B shall be either at the outlet elevation or the check dam elevation, whichever is lowest. If project area is over 200sf consider adding a tree.

- Entrance Erosion Control: Install river rock, flagstone, or similar to dissipate the energy of incoming water at entrances and ends of downspout extensions.
- Check Dams: Spacing per the PAC. Check dam ends must be keyed into the native soil a minimum of 12".
- Inspections: Call BDS IVR Inspection Line, (503) 823-7000, request 487. 3 inspections required.

#### **CONSTRUCTION REQUIREMENTS**

Mark the location of future facilities, and fence or cover facility locations after excavation. Do not allow vehicular traffic, foot traffic, material storage, or heavy equipment within 10 feet of the infiltration area except as needed to excavate, grade, and construct the facility. Do not allow entry of runoff or sediment during construction.

- DRAWING NOT TO SCALE





STORMWATER MANAGEMENT TYPICAL DETAILS FOR PRIVATE PROPERTY

**BASIN WITHOUT UNDERDRAIN** 

SW-24

## APPENDIX B RAINFALL DATA

#### A.3.2 Santa Barbara Urban Hydrograph Method

The Santa Barbara Urban Hydrograph (SBUH) method was developed by the Santa Barbara County Flood Control and Water Conservation District to determine a runoff hydrograph for an urbanized area. The SBUH method is the method approved by the City for determining runoff for volume-based facilities and rate-volume-based facilities. The SBUH method depends on several variables: the contributing area, the time of concentration (t<sub>c</sub>), the runoff curve numbers (CN), and the design storm.

#### **Contributing Area**

The contributing area is the area that drains to the stormwater facility. The contributing area must be quantified in order to evaluate the resulting site runoff.

#### **Time of Concentration**

The time of concentration,  $t_c$ , for a stormwater facility is the time for the runoff from the entire contributing area to reach the stormwater facility. The  $t_c$  is derived by calculating the overland flow time and the channelized flow time. The  $t_c$  depends on several factors, including ground slope, ground roughness, and distance of flow.

In the SBUH method, the minimum  $t_c$  that can be used is half the time step. Since the City's hyetograph uses 10-minute time steps, the minimum  $t_c$  that can be used with the City's hyetograph is 5 minutes. To calculate  $t_c$ , refer to BES's SDFDM. If the minimum calculated  $t_c$  is less than 5 minutes, use a  $t_c$  of 5 minutes.

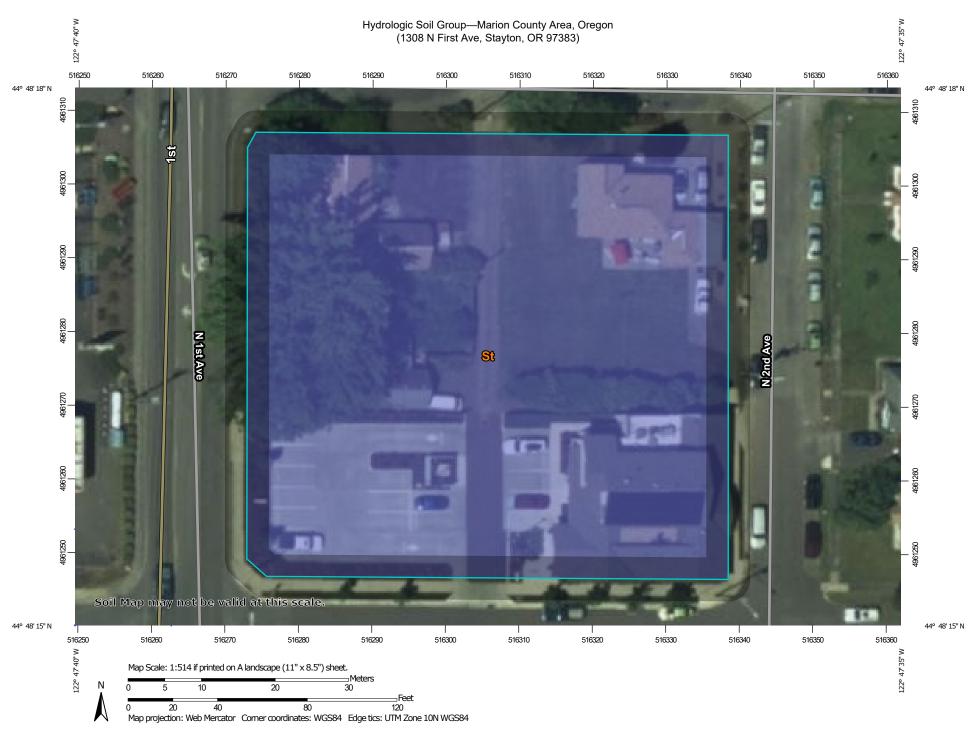
#### **Curve Numbers**

Curve numbers (CNs) were originally developed by the NRCS to translate rainfall into runoff. The higher the CN, the more runoff for a given rainfall depth. The CN changes with development; pre-development CNs in the City have been correlated to the site's soil group and post-development CNs depend upon the post-development surface (the ecoroof curve number correlates to the well-draining soils typically used for ecoroofs). The CNs shown in Table A-8 should typically be used. The SDFDM provides post-development CNs for other surfaces.

**Table A-8. Curve Numbers** 

Development Status	Area	Curve Number	
		Α	65
		В	72
Pre-development	Soil Group	С	79
		D	81
		Unidentified	81
Doct dovolopment	Imp	ervious area	98
Post-development		Ecoroof	61

## APPENDIX C SOIL DATA



#### MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:20.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: Marion County Area, Oregon Survey Area Data: Version 21, Sep 8, 2023 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: May 28, 2020—May 29. 2020 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

## **Hydrologic Soil Group**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
St	Sifton gravelly loam	В	1.0	100.0%
Totals for Area of Intere	st	1.0	100.0%	

## **Description**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

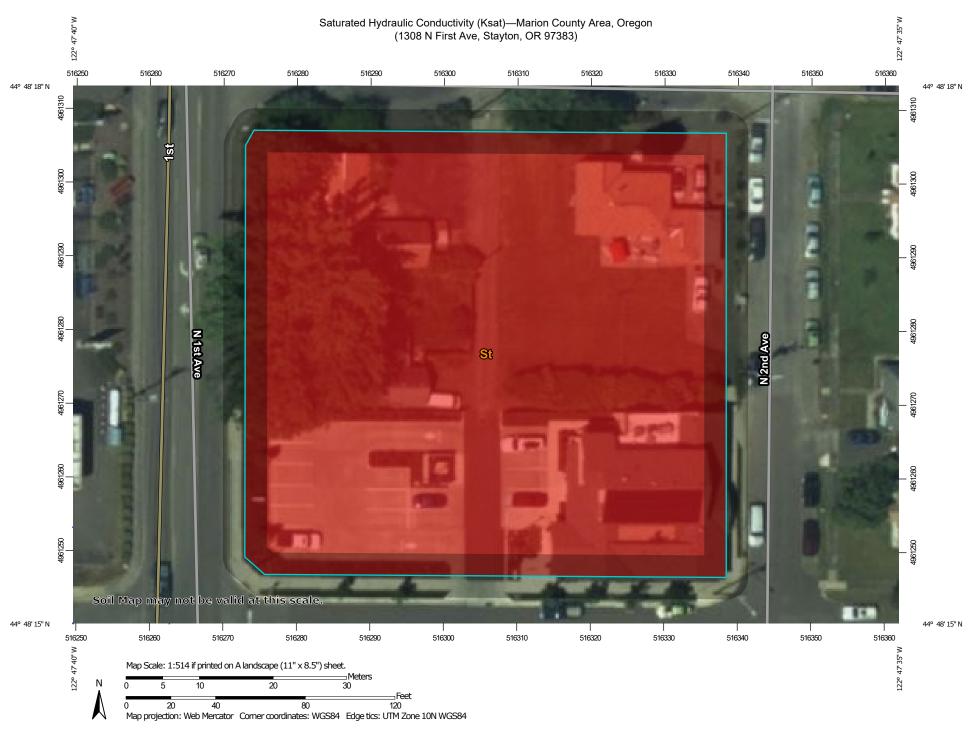
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

#### Soil Rating Polygons

= 104.9341

Not rated or not available

#### Soil Rating Lines

= 104.9341

Not rated or not available

#### **Soil Rating Points**

= 104.9341

Not rated or not available

#### Water Features



Streams and Canals

#### Transportation

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Interstate Highways

**US Routes** 

Rails



Major Roads



Local Roads

#### Background



Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Marion County Area, Oregon Survey Area Data: Version 21, Sep 8, 2023

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: May 28, 2020—May 29. 2020

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## **Saturated Hydraulic Conductivity (Ksat)**

Map unit symbol	Map unit name	• ,	micrometers second)	Acres in AOI	Percent of AOI						
St	Sifton gravelly loam	104.9341	= 14.7 in/hr	1.0	100.0%						
Totals for Area of Intere	est		_ _With FS = 4	1.0	100.0%						
			3.7 in/hr	,							

## **Description**

Saturated hydraulic conductivity (Ksat) refers to the ease with which pores in a saturated soil transmit water. The estimates are expressed in terms of micrometers per second. They are based on soil characteristics observed in the field, particularly structure, porosity, and texture. Saturated hydraulic conductivity is considered in the design of soil drainage systems and septic tank absorption fields.

For each soil layer, this attribute is actually recorded as three separate values in the database. A low value and a high value indicate the range of this attribute for the soil component. A "representative" value indicates the expected value of this attribute for the component. For this soil property, only the representative value is used.

The numeric Ksat values have been grouped according to standard Ksat class limits.

## **Rating Options**

Units of Measure: micrometers per second
Aggregation Method: Dominant Component
Component Percent Cutoff: None Specified

Tie-break Rule: Fastest Interpret Nulls as Zero: No

Layer Options (Horizon Aggregation Method): Depth Range (Weighted Average)

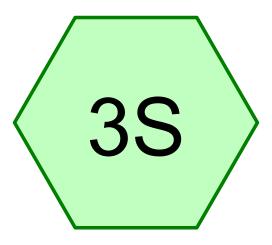
Top Depth: 0

Bottom Depth: 36

Units of Measure: Inches

## **APPENDIX D**

## PRE-DEVELOPMENT HYDROCAD MODEL



Pre-Dev









Routing Diagram for 23-231 Stayton Vet Hospital\_Pre
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## 23-231 Stayton Vet Hospital\_Pre

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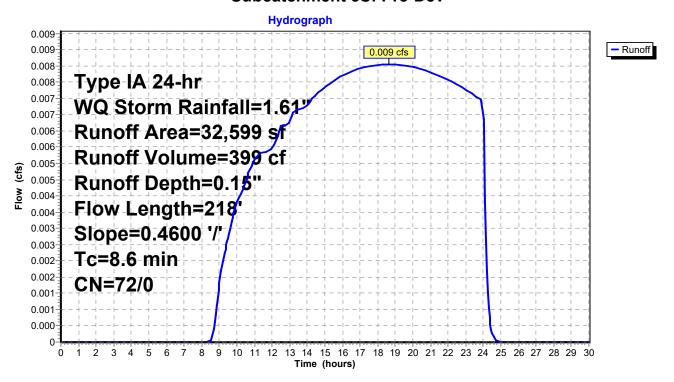
Printed 3/20/2024

## **Summary for Subcatchment 3S: Pre-Dev**

Runoff = 0.009 cfs @ 18.62 hrs, Volume= 399 cf, Depth= 0.15"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr WQ Storm Rainfall=1.61"

_	Α	rea (sf)	CN	Description					
*		32,599	72						
		32,599	72	100.00% Pe	rvious Area				
	Тс	Length	Slope	,	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	8.6	218	0.4600	0.42		Sheet Flow, Grass: Dense	n= 0.240	P2= 2.50"	



## 23-231 Stayton Vet Hospital\_Pre

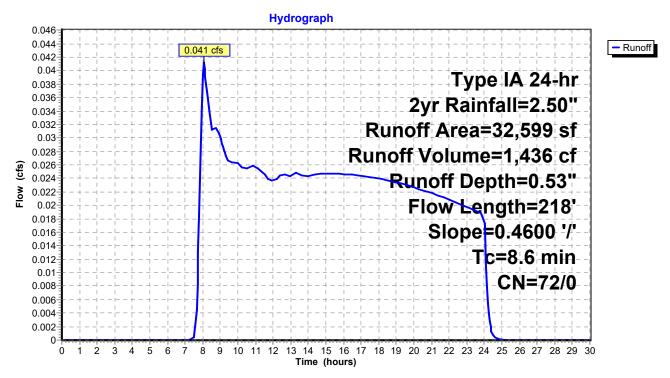
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## **Summary for Subcatchment 3S: Pre-Dev**

Runoff = 0.041 cfs @ 8.06 hrs, Volume= 1,436 cf, Depth= 0.53"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 2yr Rainfall=2.50"

_	Α	rea (sf)	CN I	Description					
*		32,599	72						
_		32,599	72	100.00% Pe	rvious Area				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	8.6	218	0.4600	0.42	•	Sheet Flow, Grass: Dense	n= 0.240	P2= 2.50"	



## 23-231 Stayton Vet Hospital Pre

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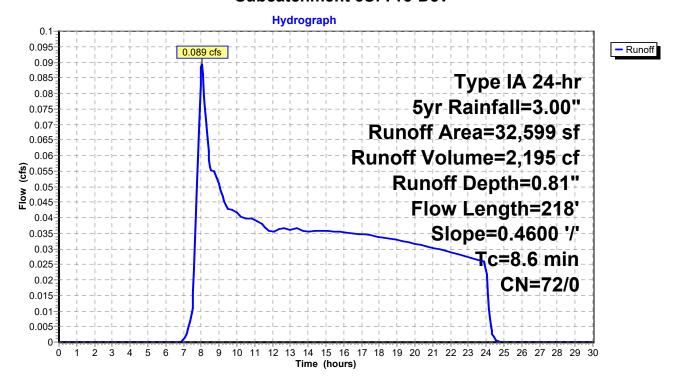
Page 4

## **Summary for Subcatchment 3S: Pre-Dev**

Runoff = 0.089 cfs @ 8.02 hrs, Volume= 2,195 cf, Depth= 0.81"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 5yr Rainfall=3.00"

_	Α	rea (sf)	CN	Description					
*		32,599	72						
		32,599	72	100.00% Pe	rvious Area				
	Tc (min)	Length (feet)	Slope (ft/ft)	,	Capacity (cfs)	Description			
	8.6	218	0.4600	0.42	, ,	Sheet Flow, Grass: Dense	n= 0.240	P2= 2.50"	



## 23-231 Stayton Vet Hospital\_Pre

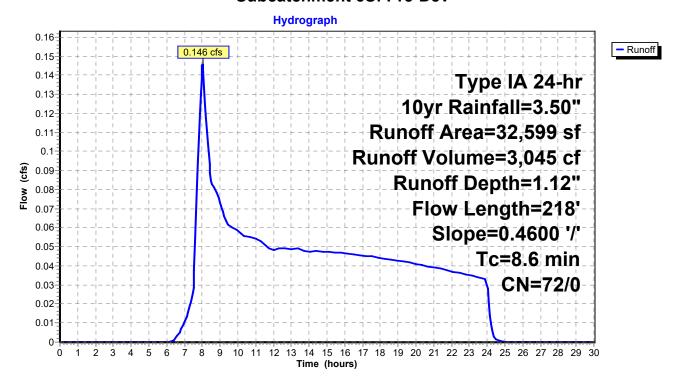
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## **Summary for Subcatchment 3S: Pre-Dev**

Runoff = 0.146 cfs @ 8.01 hrs, Volume= 3,045 cf, Depth= 1.12"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 10yr Rainfall=3.50"

_	Α	rea (sf)	CN	Description					
*		32,599	72						
		32,599	72	100.00% Pe	rvious Area				
		Length	Slope	,	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	8.6	218	0.4600	0.42		Sheet Flow, Grass: Dense	n= 0.240	P2= 2.50"	



## 23-231 Stayton Vet Hospital\_Pre

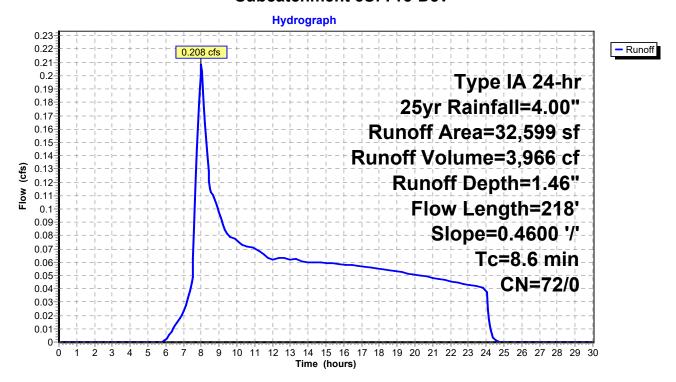
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## **Summary for Subcatchment 3S: Pre-Dev**

Runoff = 0.208 cfs @ 8.01 hrs, Volume= 3,966 cf, Depth= 1.46"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 25yr Rainfall=4.00"

	Α	rea (sf)	CN I	Description					
*		32,599	72						
		32,599	72	100.00% Pe	rvious Area				
	Tc	9	Slope	,	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	8.6	218	0.4600	0.42		Sheet Flow, Grass: Dense	n= 0.240	P2= 2.50"	



## 23-231 Stayton Vet Hospital\_Pre

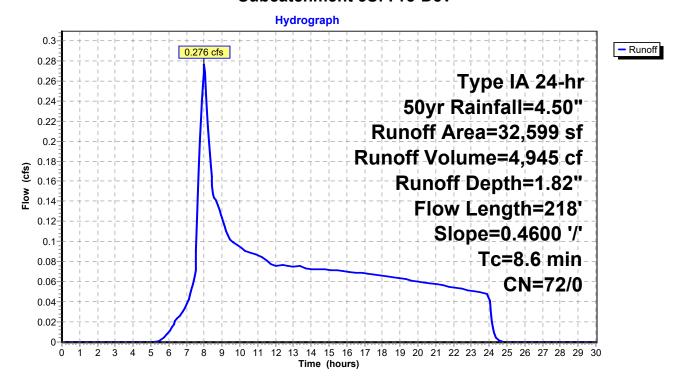
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## **Summary for Subcatchment 3S: Pre-Dev**

Runoff = 0.276 cfs @ 8.00 hrs, Volume= 4,945 cf, Depth= 1.82"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 50yr Rainfall=4.50"

	Α	rea (sf)	CN	Description					
*		32,599	72						
		32,599	72	100.00% Pe	rvious Area				
	Tc (min)	Length (feet)	Slope (ft/ft)	,	Capacity (cfs)	Description			
_	8.6	218	0.4600	0.42	, ,	Sheet Flow, Grass: Dense	n= 0.240	P2= 2.50"	



## 23-231 Stayton Vet Hospital Pre

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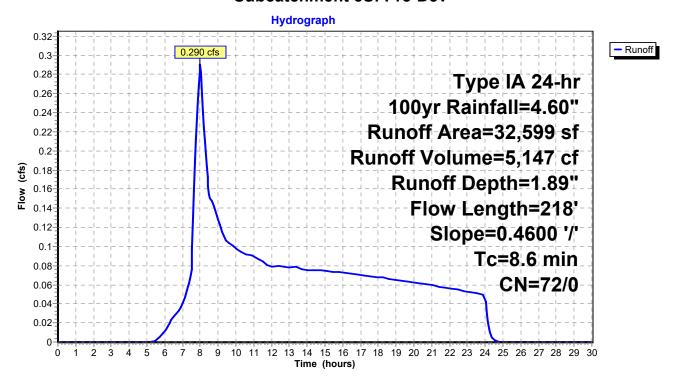
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## **Summary for Subcatchment 3S: Pre-Dev**

Runoff 0.290 cfs @ 8.00 hrs, Volume= 5,147 cf, Depth= 1.89"

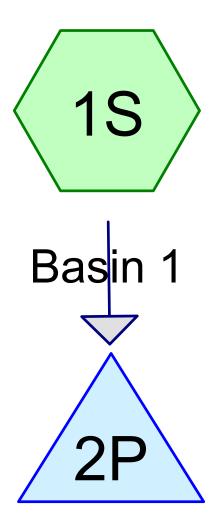
Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 100yr Rainfall=4.60"

_	Α	rea (sf)	CN	Description					
*		32,599	72						
		32,599	72	100.00% Pe	rvious Area				
		Length	Slope	,	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	8.6	218	0.4600	0.42		Sheet Flow, Grass: Dense	n= 0.240	P2= 2.50"	



## **APPENDIX E**

## POST-DEVELOPMENT HYDROCAD MODEL



## Stormwater Basin









## 23-231 Stayton Vet Hospital\_Post

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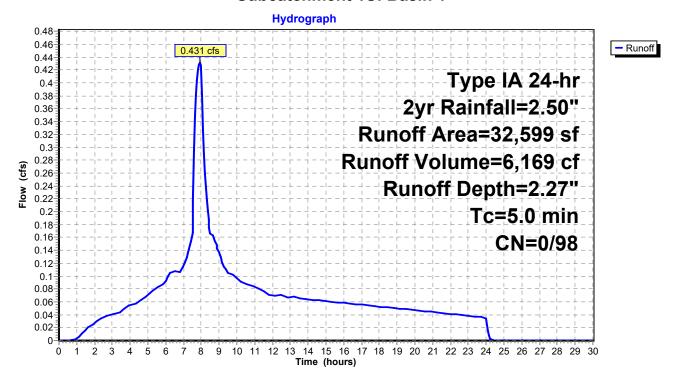
## **Summary for Subcatchment 1S: Basin 1**

Runoff = 0.431 cfs @ 7.90 hrs, Volume= 6,169 cf, Depth= 2.27"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 2yr Rainfall=2.50"

_	Α	rea (sf)	CN I	Description				
*		32,599	98 F	Pavement and Roofs				
		32,599	98 100.00% Impervious Area					
	Тс	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
_	5.0					Direct Entry,		

#### **Subcatchment 1S: Basin 1**



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# **Summary for Pond 2P: Stormwater Basin**

32,599 sf,100.00% Impervious, Inflow Depth = 2.27" for 2yr event Inflow Area = Inflow 7.90 hrs, Volume= 0.431 cfs @ 6.169 cf 7.40 hrs, Volume= 6,169 cf, Atten= 65%, Lag= 0.0 min Outflow 0.152 cfs @ Discarded = 7.40 hrs, Volume= 6,169 cf 0.152 cfs @ Primary 0.000 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 456.75' @ 8.80 hrs Surf.Area= 1,776 sf Storage= 593 cf

Plug-Flow detention time= 15.8 min calculated for 6,158 cf (100% of inflow) Center-of-Mass det. time= 15.8 min (689.6 - 673.8)

Volume	Invert	Avail.Storage	Storage Description
#1	455.50'	0 cf	37.00'W x 48.00'L x 2.17'H Overall Footprint
			3,854 cf Overall - 3,197 cf Embedded = 657 cf x 0.0% Voids
#2	455.50'	355 cf	37.00'W x 48.00'L x 1.00'H Soil MediaInside #1
			1,776 cf Overall x 20.0% Voids
#3	456.50'	1,421 cf	25.00'W x 36.00'L x 1.17'H WQ Basin Z=4.0Inside #1

1,776 cf Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	455.50'	3.700 in/hr Infiltration over Surface area
#2	Primary	457.50'	<b>24.0000" Horiz. Beehive Overflow X 0.75</b> C= 0.600
	-		Limited to weir flow at low heads

**Discarded OutFlow** Max=0.152 cfs @ 7.40 hrs HW=455.52' (Free Discharge) **1=Infiltration** (Exfiltration Controls 0.152 cfs)

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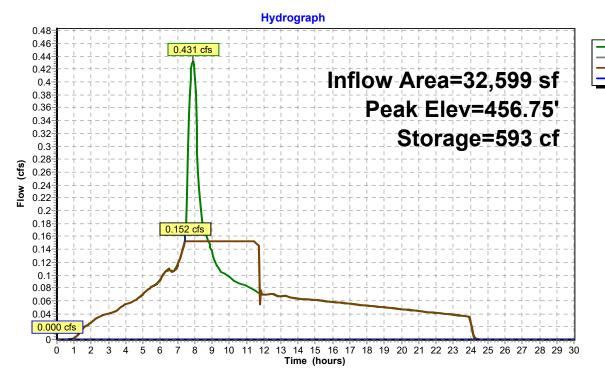
Page 4

Inflow

Outflow

Primary

Discarded



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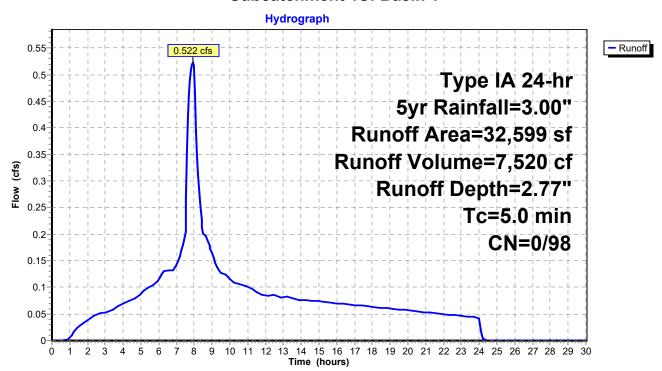
Page 5

### **Summary for Subcatchment 1S: Basin 1**

Runoff = 0.522 cfs @ 7.90 hrs, Volume= 7,520 cf, Depth= 2.77"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 5yr Rainfall=3.00"

	Α	rea (sf)	CN [	Description				
*		32,599	98 F	8 Pavement and Roofs				
		32,599	98	98 100.00% Impervious Area				
	Тс		Slope	,	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	5.0					Direct Entry,		



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### **Summary for Pond 2P: Stormwater Basin**

32,599 sf,100.00% Impervious, Inflow Depth = 2.77" for 5yr event Inflow Area = Inflow 7.90 hrs, Volume= 0.522 cfs @ 7.520 cf 7.15 hrs, Volume= 7,520 cf, Atten= 71%, Lag= 0.0 min Outflow 0.152 cfs @ Discarded = 7.15 hrs, Volume= 7,520 cf 0.152 cfs @ Primary 0.000 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 457.04' @ 9.11 hrs Surf.Area= 1,776 sf Storage= 912 cf

Plug-Flow detention time= 29.2 min calculated for 7,508 cf (100% of inflow) Center-of-Mass det. time= 29.1 min (697.4 - 668.2)

Volume	Invert	Avail.Storage	Storage Description
#1	455.50'	0 cf	37.00'W x 48.00'L x 2.17'H Overall Footprint
			3,854 cf Overall - 3,197 cf Embedded = 657 cf x 0.0% Voids
#2	455.50'	355 cf	37.00'W x 48.00'L x 1.00'H Soil MediaInside #1
			1,776 cf Overall x 20.0% Voids
#3	456.50'	1,421 cf	25.00'W x 36.00'L x 1.17'H WQ Basin Z=4.0Inside #1

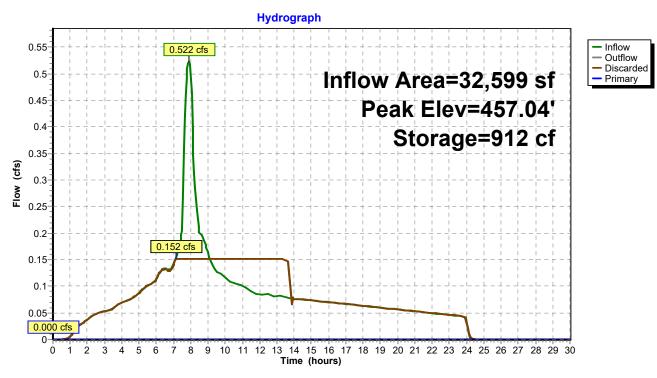
1,776 cf Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	455.50'	3.700 in/hr Infiltration over Surface area
#2	Primary	457.50'	<b>24.0000" Horiz. Beehive Overflow X 0.75</b> C= 0.600
	-		Limited to weir flow at low heads

**Discarded OutFlow** Max=0.152 cfs @ 7.15 hrs HW=455.52' (Free Discharge) **1=Infiltration** (Exfiltration Controls 0.152 cfs)

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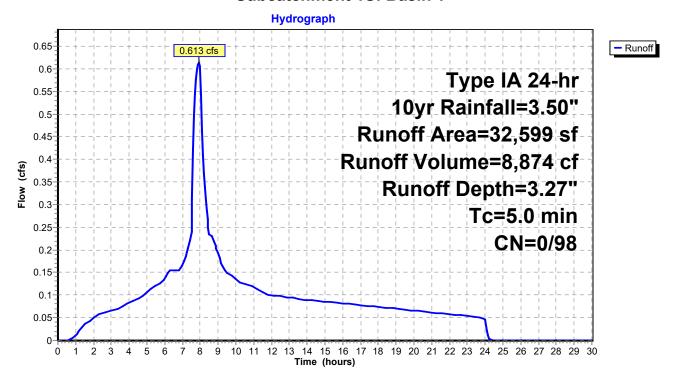
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### **Summary for Subcatchment 1S: Basin 1**

Runoff = 0.613 cfs @ 7.90 hrs, Volume= 8,874 cf, Depth= 3.27"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 10yr Rainfall=3.50"

_	Α	rea (sf)	CN	Description				
•	ŧ	32,599	98	Pavement and Roofs				
		32,599	98	3 100.00% Impervious Area				
		Length	Slope	,	. ,	Description		
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	5.0					Direct Entry		



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# **Summary for Pond 2P: Stormwater Basin**

32,599 sf,100.00% Impervious, Inflow Depth = 3.27" for 10yr event Inflow Area = Inflow 7.90 hrs, Volume= 0.613 cfs @ 8.874 cf 6.30 hrs, Volume= 8,874 cf, Atten= 75%, Lag= 0.0 min Outflow 0.152 cfs @ Discarded = 6.30 hrs, Volume= 8,874 cf 0.152 cfs @ Primary 0.000 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 457.34' @ 9.42 hrs Surf.Area= 1,776 sf Storage= 1,291 cf

Plug-Flow detention time= 50.2 min calculated for 8,859 cf (100% of inflow) Center-of-Mass det. time= 50.1 min (714.1 - 664.0)

Volume	Invert	Avail.Storage	Storage Description
#1	455.50'	0 cf	37.00'W x 48.00'L x 2.17'H Overall Footprint
			3,854 cf Overall - 3,197 cf Embedded = 657 cf x 0.0% Voids
#2	455.50'	355 cf	37.00'W x 48.00'L x 1.00'H Soil Media Inside #1
			1,776 cf Overall x 20.0% Voids
#3	456.50'	1,421 cf	25.00'W x 36.00'L x 1.17'H WQ Basin Z=4.0Inside #1
-			

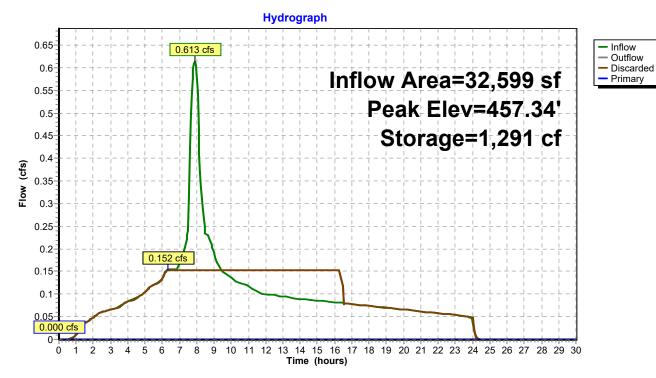
1,776 cf Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	455.50'	3.700 in/hr Infiltration over Surface area
#2	Primary	457.50'	<b>24.0000" Horiz. Beehive Overflow X 0.75</b> C= 0.600
			I imited to weir flow at low heads

**Discarded OutFlow** Max=0.152 cfs @ 6.30 hrs HW=455.52' (Free Discharge) **1=Infiltration** (Exfiltration Controls 0.152 cfs)

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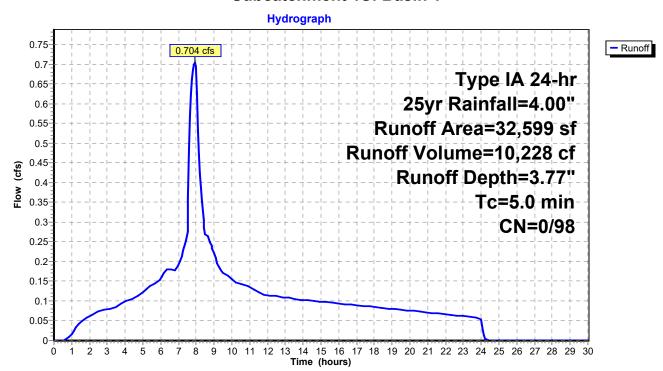
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# **Summary for Subcatchment 1S: Basin 1**

Runoff = 0.704 cfs @ 7.90 hrs, Volume= 10,228 cf, Depth= 3.77"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 25yr Rainfall=4.00"

_	Α	rea (sf)	CN	Description				
•	ŧ	32,599	98	Pavement and Roofs				
		32,599	98	3 100.00% Impervious Area				
		Length	Slope	,	. ,	Description		
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	5.0					Direct Entry		



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### **Summary for Pond 2P: Stormwater Basin**

32,599 sf,100.00% Impervious, Inflow Depth = 3.77" for 25yr event Inflow Area = Inflow 7.90 hrs, Volume= 0.704 cfs @ 10,228 cf 8.80 hrs, Volume= 10,228 cf, Atten= 65%, Lag= 54.4 min Outflow 0.247 cfs @ Discarded = 5.95 hrs, Volume= 0.152 cfs @ 9,970 cf Primary 0.095 cfs @ 8.80 hrs, Volume= 258 cf

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 457.53' @ 8.80 hrs Surf.Area= 1,776 sf Storage= 1,568 cf

Plug-Flow detention time= 68.5 min calculated for 10,211 cf (100% of inflow) Center-of-Mass det. time= 68.4 min (729.2 - 660.7)

Volume	Invert	Avail.Storage	Storage Description
#1	455.50'	0 cf	37.00'W x 48.00'L x 2.17'H Overall Footprint
			3,854 cf Overall - 3,197 cf Embedded = 657 cf x 0.0% Voids
#2	455.50'	355 cf	37.00'W x 48.00'L x 1.00'H Soil Media Inside #1
			1,776 cf Overall x 20.0% Voids
#3	456.50'	1,421 cf	25.00'W x 36.00'L x 1.17'H WQ Basin Z=4.0Inside #1
-			

1,776 cf Total Available Storage

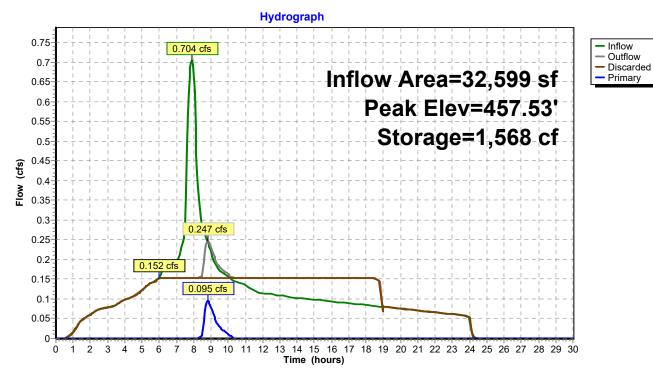
Device	Routing	Invert	Outlet Devices
#1 #2	Discarded Primary		3.700 in/hr Infiltration over Surface area 24.0000" Horiz. Beehive Overflow X 0.75 C= 0.600 Limited to weir flow at low heads

**Discarded OutFlow** Max=0.152 cfs @ 5.95 hrs HW=455.52' (Free Discharge) **1=Infiltration** (Exfiltration Controls 0.152 cfs)

Primary OutFlow Max=0.091 cfs @ 8.80 hrs HW=457.53' (Free Discharge) 2=Beehive Overflow (Weir Controls 0.091 cfs @ 0.44 fps)

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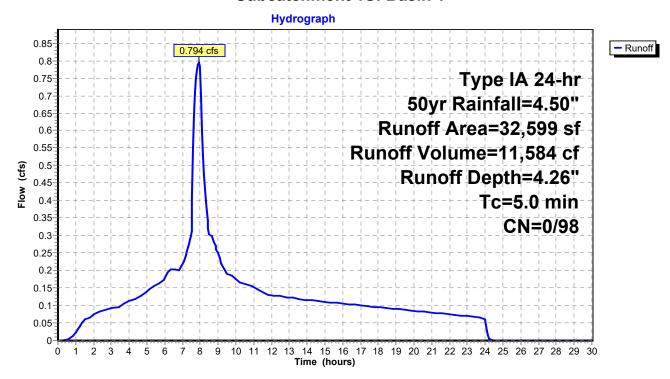
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### **Summary for Subcatchment 1S: Basin 1**

Runoff = 0.794 cfs @ 7.90 hrs, Volume= 11,584 cf, Depth= 4.26"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 50yr Rainfall=4.50"

_	Α	rea (sf)	CN I	Description			
*		32,599	98 F	Pavement and Roofs			
		32,599	98	3 100.00% Impervious Area			
	Тс	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
_	5.0					Direct Entry,	



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### **Summary for Pond 2P: Stormwater Basin**

32,599 sf,100.00% Impervious, Inflow Depth = 4.26" for 50yr event Inflow Area = Inflow 7.90 hrs, Volume= 11,584 cf 0.794 cfs @ 8.26 hrs, Volume= 11,584 cf, Atten= 45%, Lag= 21.9 min Outflow 0.435 cfs @ Discarded = 5.30 hrs, Volume= 0.152 cfs @ 10,753 cf Primary 0.283 cfs @ 8.26 hrs, Volume= 830 cf

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 457.57' @ 8.26 hrs Surf.Area= 1,776 sf Storage= 1,623 cf

Plug-Flow detention time= 73.5 min calculated for 11,564 cf (100% of inflow) Center-of-Mass det. time= 73.4 min (731.5 - 658.1)

Volume	Invert	Avail.Storage	Storage Description
#1	455.50'	0 cf	37.00'W x 48.00'L x 2.17'H Overall Footprint
			3,854 cf Overall - 3,197 cf Embedded = 657 cf x 0.0% Voids
#2	455.50'	355 cf	37.00'W x 48.00'L x 1.00'H Soil Media Inside #1
			1,776 cf Overall x 20.0% Voids
#3	456.50'	1,421 cf	25.00'W x 36.00'L x 1.17'H WQ Basin Z=4.0Inside #1
-			

1,776 cf Total Available Storage

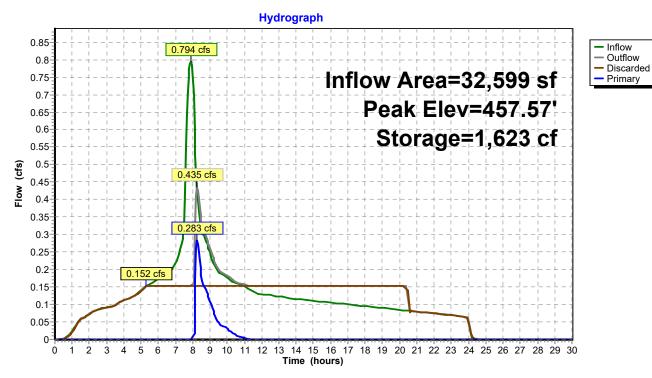
Device	Routing	Invert	Outlet Devices
#1 #2	Discarded Primary		3.700 in/hr Infiltration over Surface area 24.0000" Horiz. Beehive Overflow X 0.75 C= 0.600 Limited to weir flow at low heads

**Discarded OutFlow** Max=0.152 cfs @ 5.30 hrs HW=455.52' (Free Discharge) **1=Infiltration** (Exfiltration Controls 0.152 cfs)

Primary OutFlow Max=0.278 cfs @ 8.26 hrs HW=457.57' (Free Discharge) 2=Beehive Overflow (Weir Controls 0.278 cfs @ 0.64 fps)

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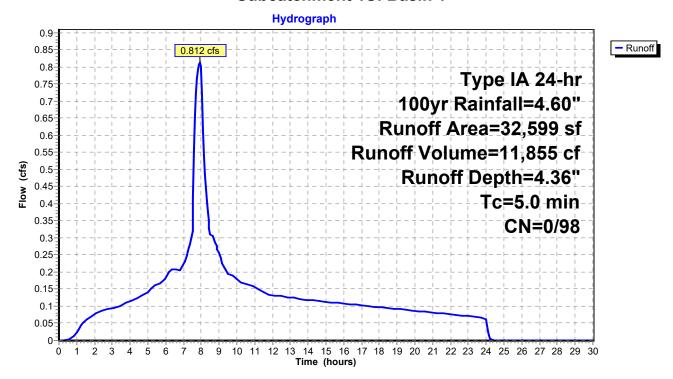
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### **Summary for Subcatchment 1S: Basin 1**

Runoff = 0.812 cfs @ 7.90 hrs, Volume= 11,855 cf, Depth= 4.36"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr 100yr Rainfall=4.60"

_	Α	rea (sf)	CN I	Description			
*		32,599	98 F	98 Pavement and Roofs			
		32,599	98	100.00% Im	pervious Ar	ea	
	Тс	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
_	5.0					Direct Entry,	



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### **Summary for Pond 2P: Stormwater Basin**

32,599 sf,100.00% Impervious, Inflow Depth = 4.36" for 100yr event Inflow Area = Inflow 7.90 hrs, Volume= 0.812 cfs @ 11,855 cf 0.487 cfs @ 8.21 hrs, Volume= 11,855 cf, Atten= 40%, Lag= 19.1 min Outflow Discarded = 5.25 hrs, Volume= 10,898 cf 0.152 cfs @ Primary 0.335 cfs @ 8.21 hrs, Volume= 956 cf

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 457.58' @ 8.21 hrs Surf.Area= 1,776 sf Storage= 1,635 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 74.4 min ( 732.0 - 657.6 )

Volume	Invert	Avail.Storage	Storage Description
#1	455.50'	0 cf	37.00'W x 48.00'L x 2.17'H Overall Footprint
			3,854 cf Overall - 3,197 cf Embedded = 657 cf x 0.0% Voids
#2	455.50'	355 cf	37.00'W x 48.00'L x 1.00'H Soil Media Inside #1
			1,776 cf Overall x 20.0% Voids
#3	456.50'	1,421 cf	25.00'W x 36.00'L x 1.17'H WQ Basin Z=4.0Inside #1
-			

1,776 cf Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	455.50'	3.700 in/hr Infiltration over Surface area
#2	Primary	457.50'	<b>24.0000" Horiz. Beehive Overflow X 0.75</b> C= 0.600
			Limited to weir flow at low heads

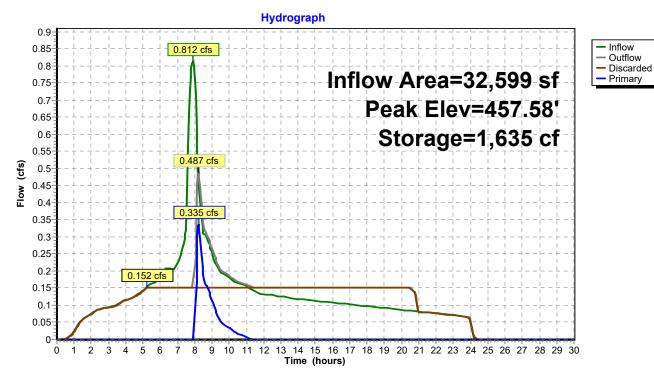
**Discarded OutFlow** Max=0.152 cfs @ 5.25 hrs HW=455.52' (Free Discharge) **1=Infiltration** (Exfiltration Controls 0.152 cfs)

Primary OutFlow Max=0.329 cfs @ 8.21 hrs HW=457.58' (Free Discharge) 2=Beehive Overflow (Weir Controls 0.329 cfs @ 0.68 fps)

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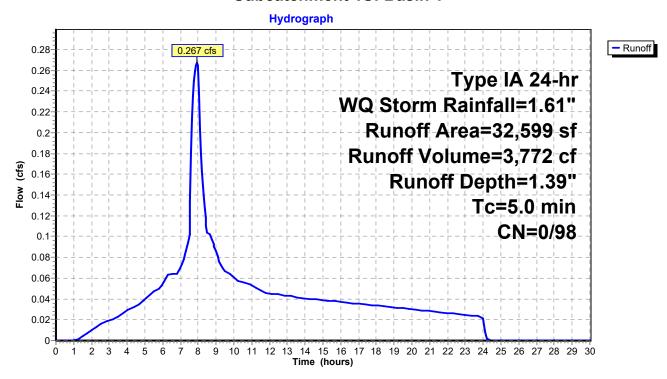
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### **Summary for Subcatchment 1S: Basin 1**

Runoff = 0.267 cfs @ 7.91 hrs, Volume= 3,772 cf, Depth= 1.39"

Runoff by SBUH method, Split Pervious/Imperv., Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Type IA 24-hr WQ Storm Rainfall=1.61"

_	Α	rea (sf)	CN	Description			
*		32,599	98	98 Pavement and Roofs			
		32,599	98	100.00% lm	pervious Ar	rea	
	Тс	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	5.0					Direct Entry,	



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# **Summary for Pond 2P: Stormwater Basin**

32,599 sf,100.00% Impervious, Inflow Depth = 1.39" for WQ Storm event Inflow Area = Inflow 7.91 hrs, Volume= 0.267 cfs @ 3,772 cf 7.60 hrs, Volume= 3,772 cf, Atten= 43%, Lag= 0.0 min Outflow 0.152 cfs @ Discarded = 7.60 hrs, Volume= 3,772 cf 0.152 cfs @ Primary 0.000 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 456.03' @ 8.24 hrs Surf.Area= 1,776 sf Storage= 188 cf

Plug-Flow detention time= 3.5 min calculated for 3,766 cf (100% of inflow) Center-of-Mass det. time= 3.5 min ( 693.9 - 690.3 )

Volume	Invert	Avail.Storage	Storage Description
#1	455.50'	0 cf	37.00'W x 48.00'L x 2.17'H Overall Footprint
			3,854 cf Overall - 3,197 cf Embedded = 657 cf x 0.0% Voids
#2	455.50'	355 cf	37.00'W x 48.00'L x 1.00'H Soil MediaInside #1
			1,776 cf Overall x 20.0% Voids
#3	456.50'	1,421 cf	25.00'W x 36.00'L x 1.17'H WQ Basin Z=4.0Inside #1

1,776 cf Total Available Storage

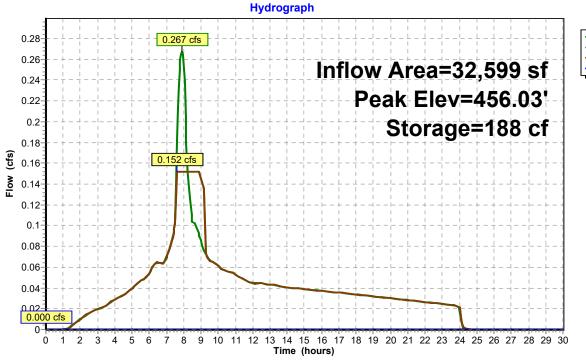
Device	Routing	Invert	Outlet Devices
#1	Discarded	455.50'	3.700 in/hr Infiltration over Surface area
#2	Primary	457.50'	<b>24.0000" Horiz. Beehive Overflow X 0.75</b> C= 0.600
			Limited to weir flow at low heads

**Discarded OutFlow** Max=0.152 cfs @ 7.60 hrs HW=455.53' (Free Discharge) **1=Infiltration** (Exfiltration Controls 0.152 cfs)

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### Pond 2P: Stormwater Basin





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